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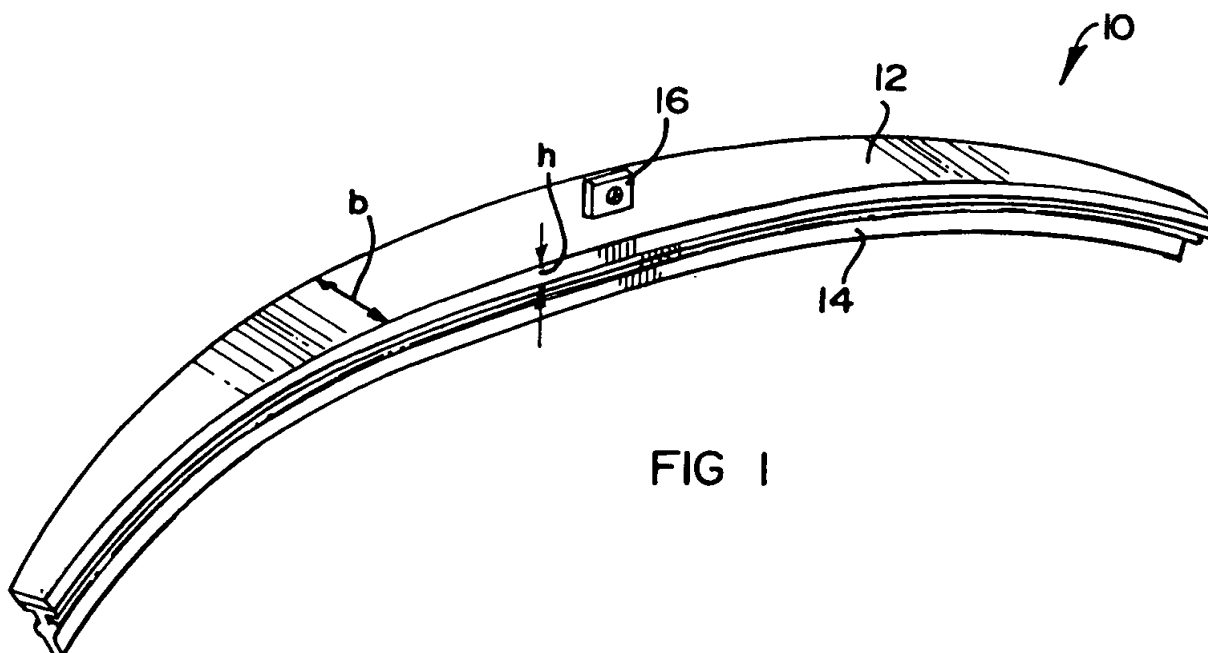
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(54) **Windscreen wiper.**

(57) A windscreen wiper (10) includes an elongate curved backbone (12) which is of a resiliently flexible material and which has a connecting formation (16) at a position intermediate its length for connection to a displacing and force applying member. The backbone (12) has a free-form curved profile in a plane, thereby to define a transverse axis perpendicular to the plane. The backbone (12) further has a suitably varying transverse cross-sectional profile along its length such that if it is clamped at its connecting formation (16) and a test force of 1N applied at a tip in a direction that is parallel to the transverse axis, the tip is displaced less than 1,0mm.



**FIG 1**

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**THIS INVENTION** relates to a windscreen wiper and more particularly to an elongate curved backbone for a windscreen wiper which is of a suitably resiliently flexible material.

According to a first aspect of the invention there is provided a windscreen wiper which includes

an elongate curved backbone which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member;

the backbone having a free-form curved profile in a plane, thereby to define a transverse axis perpendicular to the plane; and

the backbone having a suitably varying transverse cross-sectional profile along its length such that if it is clamped at its connecting formation and a test force of 1N applied at a tip in a direction that is parallel to the transverse axis, the tip is displaced less than 1,0mm.

Preferably, it is displaced less than 0,7 mm. Most preferably, it is displaced less than 0,25 mm.

The tip to which the test force is applied may be displaced a distance

$$Z_E < \left( \frac{0,7}{\ell} \right)^{0,625} \quad (1)$$

Preferably, said displacement may be

$$Z_E < \left( \frac{0,0763}{\ell} \right)^{0,625}$$

where  $\ell$  is the cantilever length of the backbone from the connecting formation to the tip to which the test force is applied and where  $Z_E$  is the displacement in mm if  $\ell$  is in metres.

The windscreen wiper may include a wiper blade attached to the backbone. The backbone may be of metal. Further, the backbone may be in the form of a single homogenous strip or in the form of a laminate.

The connecting formation may be centrally located. The backbone may be asymmetrically arranged about the connecting formation. The distance from the connecting formation to each tip may be at least 200mm.

According to a second aspect of the invention, there is provided

a windscreen wiper which includes

an elongate backbone which is curved in a plane, is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member;

the backbone defining an x-y plane, a z-axis extending perpendicularly from the x-y plane;

the backbone having a suitably varying cross-sectional profile along its length and a suitable free-form curvature, such that a double integral  $Z_T$  is less than 1,0mm, where

$$Z_T = \int_0^{\ell} \sin \left[ \int_0^x \frac{I_{zz}(x)}{R(x) I_{yy}(x)} dx \right] dx$$

and  $I_{zz}(x)$  is the moment of inertia about the z-axis at a position x along the backbone,  $R(x)$  is the radius of curvature of the backbone at position x, and  $I_{yy}(x)$  is the moment of inertia about the y-axis at position x.

Preferably  $Z_T < 0,5\text{mm}$ .

The windscreen wiper may include a wiper blade attached to the backbone.

Persons skilled in the art will appreciate that the backbone will have a concave side and a convex side, the wiper blade being attached to the concave side and the displacing and force applying member on the convex side.

The backbone may be of metal such as spring steel and may be in the form of a single homogenous strip or may be in the form of a laminate.

The connecting formation may be centrally located or the backbone may be asymmetrically arranged about the connecting formation.

The distance from the connecting formation to each tip may be at least 200mm.

Those skilled in the art will appreciate that  $I_{zz}(x)$  and  $I_{yy}(x)$  are determined by the transverse dimensions of the backbone at any position along its length. In most cases, the backbone will have a regular cross-sectional profile which may, for example, be rectangular or ellipsoidal. In most instances, the backbone will have a width and a thickness. It will be understood that the width dimension (b) will be that dimension which extends perpendicularly to the plane of curvature and the thickness (h) will be the dimension which lies in the plane of curvature.

It can be shown, with a backbone which has a rectangular cross-section at all positions along its length, that

$$I_{yy}(x) = \frac{b^3(x) * h(x)}{12}, \text{ and } (3)$$

$$I_{zz}(x) = \frac{b(x) * h^3(x)}{12} \quad (4)$$

Thus, with a rectangular cross-section,

$$Z_{TR} = \int_0^L \sin \left[ \int_0^x \frac{h^2(x)}{R(x) b^2(x)} dx \right] dx \quad \text{--- (5)}$$

The invention is now described, by way of an example, with reference to the accompanying drawings, in which:

Figure 1 is a schematic perspective view from above of a windscreen wiper in accordance with the invention;

Figure 2 is a side elevation of the windscreen wiper in an unloaded, free-form condition;

Figure 3 is a schematic sectioned view of the wiper along lines III-III in Figure 2;

Figure 4 shows schematically the axial convention utilised in this specification; and

Figure 5 shows graphically the variation in the radius of curvature of the backbone of the wiper in its free-form condition.

A symmetrical windscreen wiper in accordance with the invention is referred to generally by reference numeral 10. It includes a spring backbone 12 and a rubber wiper blade 14. The backbone 12 has a centrally located connector 16 for releasably connecting the wiper 10 to a spring loaded wiper arm (not shown). The connector 16 could be of any suitable type. The backbone 12 has suitable attachment formations (also not shown) whereby the blade 14 is securely attached to the backbone 12, or the blade 14 is glued to the backbone 12.

The spring backbone 12 is preferably made from spring steel and tapers both in width and thickness from its centre towards its free ends or tips. The backbone is pre-curved longitudinally with a predetermined radius of curvature (R) at every point in its length. The backbone 12 defines a plane, which is defined by the sheet of paper in Figure 2. As indicated in Figure 4, a median line 18 of the backbone 12 lies in the x-y plane with the x axis extending tangentially at the centre of the backbone 12. The z-axis defines a transverse axis perpendicular to the plane in which the free-form curved profile of the backbone 12 lies.

The backbone 12 has a rectangular cross-sectional profile at all points along its length. Thus, the backbone 12 has a width b and a thickness h as indicated in Figure 1. It will be appreciated that the width b is the dimension parallel to the z-axis and the thickness h is the dimension perpendicular to the tangent at each point.

The free-form radius of curvature R of the backbone 12 is indicated in Figure 2 and the variation thereof is shown in Figure 5.

In the example shown, the backbone has a total length L = 450 mm  
 a modulus of elasticity =  $207 \times 10^9$  N/m<sup>2</sup>  
 thickness at the centre of the backbone = 1,29 mm  
 thickness at the tips = 0.22 mm  
 width at the centre = 11 mm, and  
 width at the tips = 6 mm.

The backbone tapers uniformly in both thickness and width in a straight line manner from its centre to its tips.

If the wiper is securely clamped at its connector 16 and a lateral force applied at either tip, parallel to the Z-axis, of 1 N, the lateral displacement of the tip in the Z direction is 0,28 mm allowing for experimental errors.

The value of  $Z_E$  (as determined in the equation 1 above) is 2,03 mm

Similarly, if the value of  $Z_{TR}$  (from equation 5 above) is computed it will be found to be 0,28 mm.

## Claims

1. A windscreen wiper which includes  
 an elongate curved backbone which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member; the backbone having a free-form curved profile in a plane, thereby to define a transverse axis perpendicular to the plane; and

the backbone having a suitably varying transverse cross-sectional profile along its length such that if it is clamped at its connecting formation and a test force of 1N applied at a tip in a direction that is parallel to the transverse axis, the tip is displaced less than 1,0mm.

- 5 2. The windscreen wiper as claimed in Claim 1, in which said displacement is less than 0,7mm.
3. The windscreen wiper as claimed in Claim 2, in which said displacement is less than 0,25mm.
4. The windscreen wiper as claimed in Claim 1 in which said displacement
- 10 
$$Z_E < \left( \frac{0,7}{\ell} \right)^{0,625}$$
5. The windscreen wiper as claimed in Claim 4 in which said displacement
- 15 
$$Z_E < \left( \frac{0,0763}{\ell} \right)^{0,625}$$
- where  $\ell$  is the cantilever length of the backbone from the connecting formation to the tip to which the test force is applied and where  $Z_E$  is the displacement in mm if  $\ell$  is in metres.
6. The windscreen wiper as claimed in Claim 1, which includes a wiper blade attached to the backbone.
- 20 7. The windscreen wiper as claimed in Claim 1, in which the backbone is of metal.
8. The windscreen wiper as claimed in Claim 1, in which the backbone is in the form of a single homogenous strip.
- 25 9. The windscreen wiper as claimed in Claim 1, in which the backbone is in the form of a laminate.
10. The windscreen wiper as claimed in Claim 1, in which the connecting formation is centrally located.
11. The windscreen wiper as claimed in Claim 1, in which the backbone is asymmetrically arranged about
- 30 the connecting formation.
12. The windscreen wiper as claimed in Claim 1, in which the distance from the connecting formation to each tip is at least 200mm.
- 35 13. A windscreen wiper which includes an elongate backbone which is curved in a plane, is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member;
- the backbone defining an x-y plane, a z-axis extending perpendicularly from the x-y plane;
- the backbone having a suitably varying cross-sectional profile along its length and a suitable free-
- 40 form curvature, such that a double integral  $Z_T$  is less than 1,0mm, where

$$Z_T = \int_0^{\ell} \sin \left[ \int_0^x \frac{I_{zz}(x)}{R(x) I_{yy}(x)} dx \right] dx$$

and  $I_{zz}(x)$  is the moment of inertia about the z-axis at a position x along the backbone,  $R(x)$  is the radius of curvature of the backbone at position x, and  $I_{yy}(x)$  is the moment of inertia about the y-axis at position x.

- 50 14. The windscreen wiper as claimed in Claim 13, in which  $Z_T$  is less than 0,5mm.
15. The windscreen wiper as claimed in Claim 13, which includes a wiper blade attached to the backbone.
16. The windscreen wiper as claimed in Claim 13, in which the backbone is of metal.
- 55 17. The windscreen wiper as claimed in Claim 13, in which the backbone is in the form of a single homogenous strip.

18. The windscreen wiper as claimed in Claim 13, in which the backbone is in the form of a laminate.
19. The windscreen wiper as claimed in Claim 13, in which the connecting formation is centrally located.
20. The windscreen wiper as claimed in Claim 13, in which the backbone is asymmetrically arranged about the connecting formation.
21. The windscreen wiper as claimed in Claim 13, in which the distance from the connecting formation to each tip is at least 200mm.
22. The windscreen wiper as claimed in Claim 13, in which the backbone has a regular cross-sectional profile.
23. The windscreen wiper as claimed in Claim 22, which has a rectangular cross-section with the backbone having a width dimension  $b(x)$ , a thickness dimension  $h(x)$  and a radius of curvature  $R(x)$  at each point  $x$  along its length and in which

$$Z_{TR} = \int_0^{\ell} \sin \left[ \int_0^x \frac{h^2(x)}{R(x) b^2(x)} dx \right] dx$$

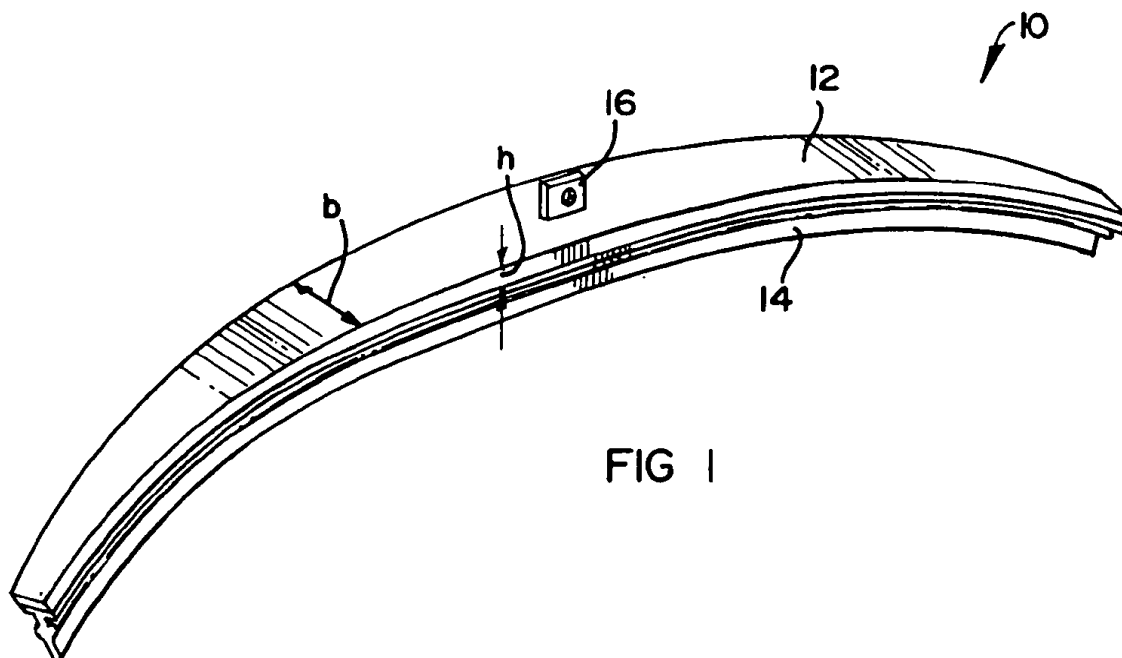


FIG 1

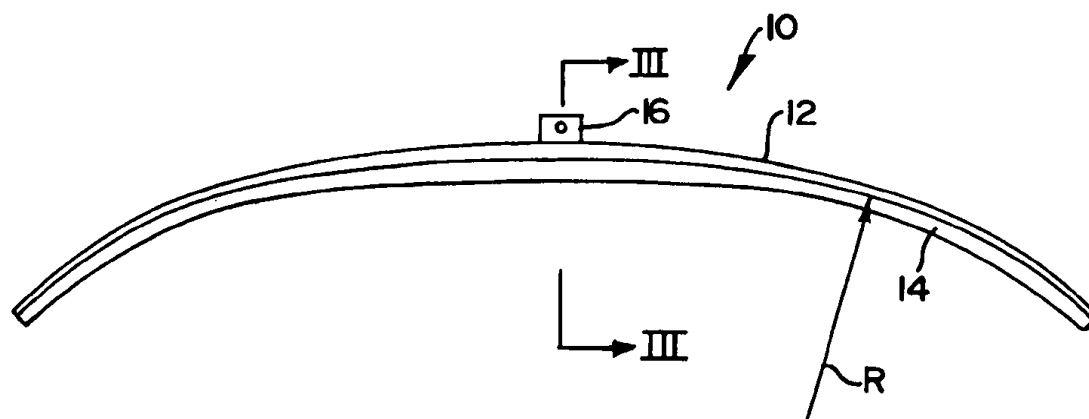


FIG 2

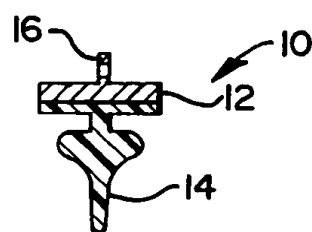


FIG 3

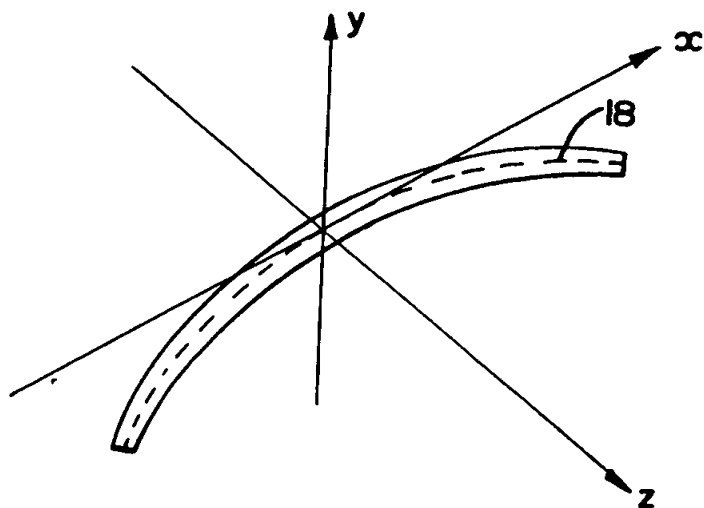


FIG 4

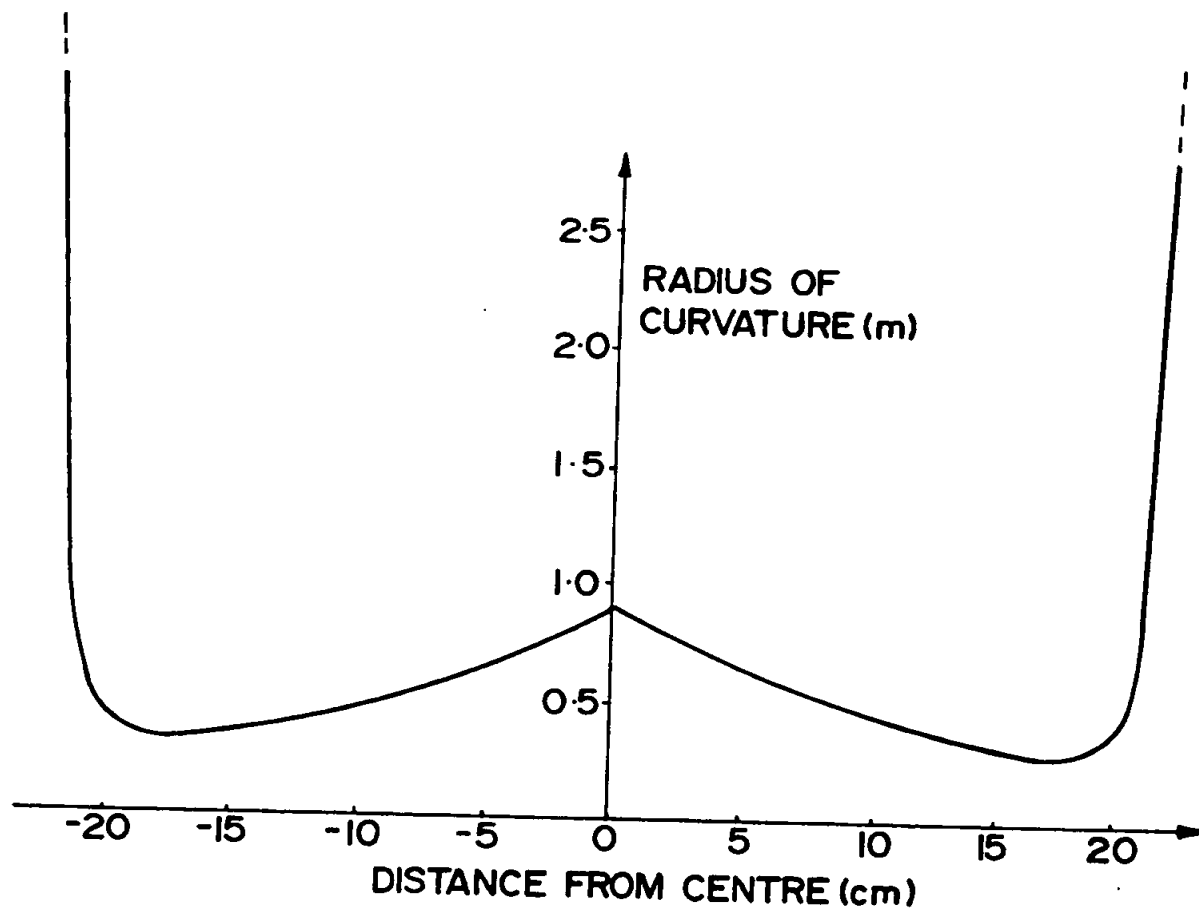


FIG 5



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# EUROPEAN SEARCH REPORT

Application Number

EP 93 30 8427

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. CL.5)
A	GB-A-1 012 902 (APPEL) * the whole document *	1, 13	B60S1/38
P, A	EP-A-0 528 643 (ANGLO AMERICAN INDUSTRIAL) * the whole document *	1, 13	
			TECHNICAL FIELDS SEARCHED (Int. CL.5)
			B60S
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 19 JANUARY 1994	Examiner BLURTON M.D.
<p><b>CATEGORY OF CITED DOCUMENTS</b></p> <p>X : particularly relevant if taken alone  Y : particularly relevant if combined with another document of the same category  A : technological background  O : non-written disclosure  P : intermediate document</p> <p>T : theory or principle underlying the invention  E : earlier patent document, but published on, or after the filing date  D : document cited in the application  L : document cited for other reasons  @ : member of the same patent family, corresponding document</p>			

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